

# Electronics Cooling Cheat Sheet<sup>1</sup>

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## Introduction

Heat conduction equation / Fourier's law

( $A$ : area,  $T$ : temperature,  $[\dot{Q}] = \text{W}$ ):

$$\dot{Q}_{\text{cond}} = -kA \frac{dT}{dx}$$

Thermal conductivity  $k$ :

$$[k] = \frac{\text{W}}{\text{m} \cdot \text{K}}$$

Convection heat flow ( $A_s$ : surface area,  $T_s$ : surface temperature,  $T_{\text{amb}}$ : ambient):

$$\dot{Q}_{\text{conv}} = hA_s \cdot (T_s - T_{\text{amb}})$$

Heat transfer coefficient  $h$ :

$$[h] = \frac{\text{W}}{\text{m}^2 \cdot \text{K}}$$

Forced convection over flat plate ( $U$ : air speed,  $[U] = \frac{\text{m}}{\text{s}}$ ,  $L$ : length of plate,  $[L] = \text{m}$ ):

- Laminar flow:  $h = 3.9 \cdot \sqrt{\frac{U}{L}}$
- Turbulent flow:  $h = 5.5 \cdot \left(\frac{U^4}{L}\right)^{1/5}$

Natural convection from vertical flat plate ( $L$ : height of plate,  $[L] = \text{m}$ ,  $T_s$ : surface temperature,  $T_{\text{amb}}$ : ambient temperature):

- Laminar flow:  $h = 1.4 \cdot \left(\frac{T_s - T_{\text{amb}}}{L}\right)^{1/4}$
- Turbulent flow:  $h = 1.1 \cdot (T_s - T_{\text{amb}})^{1/3}$

Radiation heat transfer ( $\varepsilon$ : surface emissivity,  $[\varepsilon] = 1$ ,

$\sigma = 5.67 \cdot 10^{-8} \frac{\text{W}}{\text{m}^2 \text{K}^4}$ : Stefan-Boltzmann constant,

$A_s$ : surface area,  $T_s$ : surface temperature,

$T_{\text{surr}}$ : surrounding temperature,  $[T_s] = [T_{\text{surr}}] = \text{K}$ ):

$$\dot{Q}_{\text{rad}} = \varepsilon \sigma A_s \cdot (T_s^4 - T_{\text{surr}}^4) = h_{\text{rad}} A_s \cdot (T_s - T_{\text{surr}})$$

## Heat losses

Joule's law:

$$P = V \cdot I = R \cdot I^2 = \frac{V^2}{R}$$

Average IGBT conduction loss:

$$P_{\text{avg}} = u_{\text{ce},0} \cdot I_{\text{c,avg}} + r_c \cdot I_{\text{c,rms}}^2$$

Average diode conduction loss:

$$P_{\text{avg}} = u_{\text{D},0} \cdot I_{\text{D,avg}} + r_{\text{D}} \cdot I_{\text{D,rms}}^2$$

IGBT switching loss:

- $E_{\text{on}} = \sum_{i=1}^n k_{\text{on}} \cdot i_{\text{IGBT}}(t_i)$
- $E_{\text{off}} = \sum_{i=1}^n k_{\text{off}} \cdot i_{\text{IGBT}}(t_i)$
- $P_{\text{sw}} = \frac{1}{T} (E_{\text{on}} + E_{\text{off}})$

Diode switching loss:

- $E_{\text{rr}} = \sum_{i=1}^n k_{\text{rr}} \cdot i_{\text{Diode}}(t_i)$
- $P_{\text{rr}} = \frac{E_{\text{rr}}}{T}$

## Thermal resistance networks

Thermal resistance  $R_{\text{th}}$ :

- $\dot{Q} = \frac{1}{R_{\text{th}}} \cdot \Delta T$
- $[R_{\text{th}}] = \frac{\text{K}}{\text{W}}$

Thermal resistivity  $r_{\text{th}}$  ( $[\dot{q}] = \frac{\text{W}}{\text{m}^2}$ ):

- $\dot{q} = \frac{1}{r_{\text{th}}} \cdot \Delta T$
- $[r_{\text{th}}] = \frac{\text{K} \cdot \text{m}^2}{\text{W}}$

Thermal resistance of conduction ( $t$ : thickness,  $k$ : thermal conductivity,  $A$ : area):

$$R_{\text{th,cond}} = \frac{t}{kA} = \frac{r_{\text{th}}}{A}$$

Thermal resistivity of conduction ( $t$ : thickness,  $k$ : thermal conductivity):

$$r_{\text{th,cond}} = \frac{t}{k}$$

Thermal resistance of convection ( $h$ : heat transfer coefficient,  $A_s$ : surface area):

$$R_{\text{th,conv}} = \frac{1}{hA_s}$$

Conversion of Celcius temperatures to Kelvin:

$$\frac{T}{\text{K}} = \frac{\vartheta}{\text{°C}} + 273.15$$

Radiation heat transfer coefficient ( $[T_s] = [T_{\text{surr}}] = \text{K}$ ):

$$h_{\text{rad}} = \varepsilon \sigma (T_s^2 + T_{\text{surr}}^2)(T_s + T_{\text{surr}})$$

Thermal resistance of radiation:

$$R_{\text{th,rad}} = \frac{1}{h_{\text{rad}}A}$$

Modified heat transfer coefficient ( $[T_s] = [T_{\text{surr}}] = \text{K}$ ):

$$h'_{\text{rad}} = \frac{\varepsilon \sigma (T_s^4 - T_{\text{surr}}^4)}{T_s - T_{\text{amb}}}$$

Modified conduction thermal resistance:

$$R'_{\text{th,rad}} = \frac{1}{h'_{\text{rad}} \cdot A}$$

$N$  thermal resistances in series:

$$R_{\text{th,tot}} = \sum_{i=1}^N R_{\text{th},i}$$

$N$  thermal resistances in parallel:

$$\frac{1}{R_{\text{th,tot}}} = \sum_{i=1}^N \frac{1}{R_{\text{th},i}}$$

Effective normal thermal conductivity of a PCB ( $t$ : total thickness,  $t_e$ : total thickness of epoxy layers,  $t_c$ : total thickness of copper layers,  $k_e$ : thermal conductivity of epoxy,  $k_c$ : thermal conductivity of copper):

$$k_n = \frac{t}{\frac{t_e}{k_e} + \frac{t_c}{k_c}}$$

Effective planar thermal conductivity of a PCB:

$$k_p = \frac{k_e t_e + k_c t_c}{t}$$

Heat spreading:

- $A_1$ : heat source area,  $A_2$ : heat spreader area
- $k$ : thermal conductivity of heat spreader material
- $t$ : heat spreader thickness
- $h_{\text{eff}}$ : effective heat transfer coefficient
- $r_1 = \sqrt{\frac{A_1}{\pi}}$ ,  $r_2 = \sqrt{\frac{A_2}{\pi}}$
- $\varepsilon = \frac{r_1}{r_2}$
- $\tau = \frac{t}{r_2}$
- $Bi = \frac{h_{\text{eff}} \cdot r_2}{k}$
- $\lambda = \pi + \frac{1}{\varepsilon \sqrt{\pi}}$
- $\phi = \frac{\tanh(\lambda \tau) + \frac{\lambda}{Bi}}{1 + \frac{\lambda}{Bi} \tanh(\lambda \tau)}$
- $R_{\text{th,sp}} = \frac{(1-\varepsilon)\phi}{\pi k r_1}$

<sup>1</sup><https://github.com/m-thu/sandbox/blob/master/electronics-cooling.tex>

## Heat Sinks

Heat sink parameters:

- $A_c$ : cross sectional area of one fin ( $[A_c] = \text{m}^2$ )
- $P$ : perimeter of fin cross-section ( $[P] = \text{m}$ )
- $c$ : fin length
- $k$ : thermal conductivity of heatsink material
- $A_b$ : base plate area
- $n_f$ : number of fins

Thermal resistance of heat sink (with *adiabatic approximation*):

- Corrected fin length:  $c_c = c + \frac{A_c}{P}$
- $a = \sqrt{\frac{hP}{kA_c}}$ ,  $[a] = \frac{1}{\text{m}}$
- Fin efficiency:  $\eta_f = \frac{\tanh(a \cdot c_c)}{a \cdot c_c}$
- Fin surface area:  $A_f = P \cdot c_c$
- Total heat sink area:  $A_{\text{tot}} = n_f A_f + A_b - n_f A_c$
- Heat sink efficiency:  $\eta_{\text{hs}} = 1 - \frac{n_f A_f}{A_{\text{tot}}} (1 - \eta_f)$
- $\Rightarrow R_{\text{hs,conv}} = \frac{1}{\eta_{\text{hs}} A_{\text{tot}} h}$

Caloric thermal resistance ( $c_p$ : specific heat of fluid,  $[c_p] = \frac{\text{J}}{\text{kg} \cdot \text{K}}$ ,

$\dot{V}$ : volume flow rate,  $[\dot{V}] = \frac{\text{m}^3}{\text{s}}$ ,  $\rho$ : density,  $[\rho] = \frac{\text{kg}}{\text{m}^3}$ ):

- Flow cross section:  $A_{\text{flow}}$
- Air speed:  $U_{\text{air}}$ ,  $[U] = \frac{\text{m}}{\text{s}}$
- Volume flow rate:  $\dot{V} = U_{\text{air}} \cdot A_{\text{flow}}$
- Mass flow rate:  $\dot{m} = \dot{V} \cdot \rho$
- $\Rightarrow R_{\text{hs,cal}} = \frac{1}{2\dot{m}c_p} = \frac{1}{2\dot{V}\rho c_p}$

Effective heat transfer coefficient (for spreading resistance):

$$h_{\text{eff}} = \frac{1}{(R_{\text{hs,conv}} + R_{\text{hs,cal}}) \cdot A_b}$$

Linear fit for fan curve ( $p_{\text{max}}$ : maximum pressure when fan is completely blocked,  $[p_{\text{max}}] = \text{Pa}$ ,  $\dot{V}_{\text{max}}$ : maximum volume flow rate when fan is unobstructed,  $[\dot{V}_{\text{max}}] = \frac{\text{m}^3}{\text{s}}$ ):

$$\Delta p_{\text{fan}}(\dot{V}) = p_{\text{max}} - \frac{p_{\text{max}}}{\dot{V}_{\text{max}}} \cdot \dot{V}$$

Heat sink parameters:

- $c$ : fin length
- $s$ : fin spacing
- $n_f$ : number of fins
- $n = n_f - 1$ : number of channels
- $L$ : length of heatsink (in flow direction)

Hydraulic diameter:

$$d_h = \frac{2sc}{s+c}$$

Fan pressure drop with laminar flow ( $\rho$ : air density):

$$\Delta p_{\text{lam}}(\dot{V}) = 1.5 \frac{32\rho\nu L}{n(sc)d_h^2} \cdot \dot{V}$$

Fan operating point (laminar flow):

$$\Delta p_{\text{fan}}(\dot{V}) = \Delta p_{\text{lam}} \curvearrowright \dot{V} \curvearrowright p$$

Reynolds number ( $\nu$ : kinematic viscosity,  $[\nu] = \frac{\text{m}^2}{\text{s}}$ ):

$$Re = \frac{2\dot{V}}{n(s+c)\nu}$$

Flow type:

- $Re < 2300$ : laminar flow
- $Re > 2300$ : turbulent flow

Nusselt number ( $Pr$ : Prandtl's number,  $[Pr] = 1$ ,  $[Nu] = 1$ ):

- $X = \frac{L}{d_h Re_{\text{lam}} Pr}$
- $Nu_{\text{lam}} = \frac{3.657 \left[ \tanh\left(2.264 \cdot X^{1/3} + 1.7 \cdot X^{2/3}\right) \right]^{-1} + \frac{0.0499}{X} \tanh(X)}{\tanh\left[2.432 \cdot Pr^{1/6} \cdot X^{1/6}\right]}$

Heat transfer coefficient of the heatsink ( $k_{\text{air}}$ : thermal conductivity of air):

$$h = \frac{Nu_{\text{lam}} \cdot k_{\text{air}}}{d_h}$$